Oral presentation | Reduced order models Reduced order models-II Mon. Jul 15, 2024 2:00 PM - 4:00 PM Room C

# [2-C-02] A hybrid-fidelity model for floating wave energy converters \*Michel Bergmann<sup>1,2</sup>, Beatrice Battisti<sup>3</sup> (1. Inria, Memphis team, 200 avenue de la vielle tour, 33450

\*Michel Bergmann<sup>1,2</sup>, Beatrice Battisti<sup>3</sup> (1. Inria, Memphis team, 200 avenue de la vielle tour, 33450 Talence, France., 2. Institut de Mathématiques de Bordeaux, 351, cours de la libération, 33405 Talence, France, 3. Department of Mechanical and Aerospace Engineering, Politecnico di Torino, Torino, Italy.) Keywords: Multi-fidelity numerical model, Wave energy converter, Domain decomposition

# A hybrid-fidelity model for floating wave energy converters

Michel Bergmann & Beatrice Battisti

Institut de Mathématiques de Bordeaux Memphis Project-Team, Inria Bordeaux - Sud Ouest Talence, France

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Ínría

Renewable Energies Context and motivations

General problem and flow configuration



Source: Politecnico di Torino & Marine Offshore renewable energy

# General problem and flow configuration



► Incompressible bi-fluid Navier-Stokes equations (to avoid surface fitted-grids)

$$\begin{aligned} \frac{\partial \boldsymbol{u}}{\partial t} + (\boldsymbol{u} \cdot \boldsymbol{\nabla})\boldsymbol{u} &= -\frac{1}{\rho}\boldsymbol{\nabla}p + \frac{1}{\rho}\boldsymbol{\nabla} \cdot \boldsymbol{\mu}\left(\boldsymbol{\nabla}\boldsymbol{u} + (\boldsymbol{\nabla}\boldsymbol{u})^{T}\right) + \boldsymbol{g}, \\ \boldsymbol{\nabla} \cdot \boldsymbol{u} &= 0, \\ \frac{\partial \alpha}{\partial t} + \boldsymbol{u} \cdot \boldsymbol{\nabla}\alpha &= 0 \implies \rho = \rho_{a} + (\rho_{w} - \rho_{a})H(\alpha), \ \boldsymbol{\mu} &= \mu_{a} + (\mu_{w} - \mu_{a})H(\alpha) \\ + \text{IC and BCs (wave imposed on the gray zone).} \end{aligned}$$

 $\hookrightarrow$  Too costly!  $\Rightarrow$  we can only afford few numerical simulations! (how to select??)

Reduced Order Models reduced basis, asymptotic models or simplified models

Need to reduce the CPU costs

# The Full Order Models are almost never used alone for wind or marine energy applications ⇒ large CPU costs, multiscale problem, optimization

- ► Simplified mathematical models (invariance-asymptotic)
- $\hookrightarrow$  Shallow Water Equations, Boussinesq, etc (post doc Umberto Bosi)
- $\hookrightarrow$  Inviscid incompressible Navier-Stokes equations (PhD Caroline Le Guern)

# ► Simplified numerical models based on data (only polar curves for 2D airfoils)

- $\hookrightarrow$  Actual blades are modeled using <u>extra Volume Forces based on data</u>
- $\hookrightarrow$  <u>Actuator lines</u>: (post doc Nishant Kumar)

► Model Order Reduction based on data (primitive variables)

→ Proper Orthogonal Decomposition Reduced Order Model (PhD Beatrice Battisti)

$$\boldsymbol{U}(\boldsymbol{x}, t) = \sum_{i=1}^{N} a_i(t) \boldsymbol{\Phi}_i(\boldsymbol{x}) \quad \boldsymbol{U} = \boldsymbol{u}, \boldsymbol{v}, \boldsymbol{w}, \boldsymbol{p}, \boldsymbol{\rho}, \boldsymbol{\mu}, \dots$$

#### **Proper Orthogonal Decomposition (POD), Lumley (1967)**

 $\triangleright$  Look for the flow realization  $\Phi(X)$  that is "the closest" in an average sense to realizations U(X).

 $(\boldsymbol{X} = (\boldsymbol{x}, t) \in \mathcal{D} = \Omega \times \mathbb{R}^+)$ 

 $\triangleright \Phi(X)$  solution of problem:

$$\max_{\mathbf{\Phi}} \langle |(\boldsymbol{U}, \boldsymbol{\Phi})|^2 \rangle, \quad \|\boldsymbol{\Phi}\|^2 = 1.$$

▷ Optimal convergence in  $L^2$  norm de  $\Phi(X)$ ⇒ Dynamical reduction possible.



Lumley J.L. (1967) : The structure of inhomogeneous turbulence. *Atmospheric Turbulence and Wave Propagation*, ed. A.M. Yaglom & V.I. Tatarski, pp. 166-178.

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# Low dimensional subspace

 $\triangleright$  Equivalent with Fredholm equation, R(X, X') is space-time correlation tensor

$$\int_{\mathcal{D}} R_{ij}(\boldsymbol{X}, \boldsymbol{X'}) \Phi_n^{(j)}(\boldsymbol{X'}) \, d\boldsymbol{X'} = \lambda_n \Phi_n^{(i)}(\boldsymbol{X}) \qquad n = 1, ..., N_s$$

▷ Snapshots method, Sirovich (1987) :

$$\int_T C(t,t')a_n(t')\,dt' = \lambda_n a_n(t)$$

 $\triangleright$  POD basis  $\Phi(X)$  with  $N_s$  snapshots

$$oldsymbol{U}(oldsymbol{x},t) = \sum_{n=1}^{N_s} a_n(t) oldsymbol{\Phi}_n(oldsymbol{x}),$$
  
 $\widetilde{oldsymbol{U}}(oldsymbol{x},t) = \sum_{n=1}^{N_r} a_n(t) oldsymbol{\Phi}_n(oldsymbol{x}), \quad ext{with} \quad N_r \ll N_s$ 



 $\triangleright$  POD basis  $\Phi(X)$  highly depends on the snapshots (sampling problem)

Sirovich L. (1987) : Turbulence and the dynamics of coherent structures. Part 1,2,3 *Quarterly of Applied Mathematics*, **XLV** N° 3, pp. 561–571.

# Full Order Model and POD reduced order model

### ► A POD ROM in the whole computational domain?

- $\hookrightarrow$  How to deal with complex body deformations and motions?
- $\hookrightarrow$  Is a single POD ROM accurate in the whole domain?
- $\hookrightarrow$  Is the same accuracy necessary in the whole domain?

# ▶ Past observations, for academic to industrial configurations

- $\hookrightarrow$  Large POD projection errors in the vicinity of the obstacles
- $\hookrightarrow$  Low POD projection errors elsewhere

# ► Proposed solution

 $\hookrightarrow$  Couple FOM in the vicinity of the obstacles with POD ROM elsewhere

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	Reduced Order Models	POD reduced basis		

# General configuration



 $\hookrightarrow$  The POD basis functions  $\{\Phi_i\}_{i=1}^N$  are **learned from data** (2nd part of this talk)  $\hookrightarrow$  The POD coefficients  $\{a_i\}_{i=1}^N$  can be obtained by **optimization (Galerkin-free)** 

# Generalized coordinates $\{a\}_{i=1}^{N_r}$

(a) (Petrov-) Galerkin Reduced Order Model  $(N_r \ll N_s)$ 

$$\boldsymbol{U} = \boldsymbol{U}_{g} + \sum_{n=1}^{N_{r}} \boldsymbol{a}_{n} \boldsymbol{\Phi}_{n}, \quad \text{POD on "scaled" } \boldsymbol{U} = \left(\boldsymbol{u}, \frac{1}{\rho}, \mu, p\right)^{T} \\ \left(\boldsymbol{\Phi}_{i}^{\boldsymbol{u}}, \frac{\partial \boldsymbol{u}}{\partial t} + (\boldsymbol{u} \cdot \boldsymbol{\nabla})\boldsymbol{u}\right) = \left(\boldsymbol{\Phi}_{i}^{\boldsymbol{u}}, -\frac{1}{\rho}\boldsymbol{\nabla}p + \frac{1}{\rho}\boldsymbol{\nabla}\cdot\boldsymbol{\mu}(\boldsymbol{\nabla}\boldsymbol{u} + \boldsymbol{\nabla}\boldsymbol{u}^{T})\right).$$

► Dynamical system

$$\begin{cases} \frac{d a_i(t)}{d t} = \mathcal{A}_i + \sum_{j=1}^{N_r} \mathcal{B}_{ij} a_j(t) + \sum_{j=1}^{N_r} \sum_{k=1}^{N_r} \mathcal{C}_{ijk} a_j(t) a_k(t) + \sum_{j=1}^{N_r} \sum_{k=1}^{N_r} \sum_{l=1}^{N_r} \mathcal{D}_{ijkl} a_j(t) a_k(t) a_l(t) \\ a_i(0) = (\boldsymbol{u}(\boldsymbol{x}, 0), \boldsymbol{\Phi}_i(\boldsymbol{x})). \end{cases}$$

 $\hookrightarrow$  Costly  $\Rightarrow$  The 4<sup>th</sup> order tensor involved is to costly to build and to solve!)

- $\hookrightarrow$  If number of modes is 100  $\Rightarrow$  size of 100 millions...
- $\hookrightarrow$  Not compatible with Model Order Reduction
- $\hookrightarrow$  Hyperreduction: Not compatible with "industrial" numerical solver

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	Reduced Order Models	POD reduced basis		
Reduced Order Model				

# **Generalized coordinates** $\{a\}_{i=1}^{N_r}$

# (b) Galerkin-free Reduced Order Model

What variables?  $\Rightarrow$  whose are measured at inflow AND required for FOM BCs

Velocity: 
$$\widetilde{\boldsymbol{u}} = \boldsymbol{u}_g + \sum_{i=1}^{N_r} \hat{\boldsymbol{u}}_i \boldsymbol{\Phi}_i,$$
  
Color function (VOF, LS):  $\widetilde{\alpha} = \alpha_g + \sum_{i=1}^{N_r} \hat{\alpha}_i \Psi_i \implies \rho, \mu.$ 

The functions  $\boldsymbol{u}_g$  and  $\alpha_g$  can be snapshots average, or any desired functions  $\hookrightarrow \{\hat{\boldsymbol{u}}\}_{i=1}^{N_r} \leftarrow \text{Least squares minimization of } \|\boldsymbol{u}_h - \widetilde{\boldsymbol{u}}\|_2 \text{ in "gray" domains } \Omega_o \cup \Omega_f,$   $\hookrightarrow \{\hat{\alpha}\}_{i=1}^{N_r} \leftarrow \text{Least squares minimization of } \|\alpha_h - \widetilde{\alpha}\|_2 \text{ in "gray" domains } \Omega_o \cup \Omega_f.$  $\hookrightarrow \text{More stable than classical Galerkin projection since HD informations are involved}$ 

#### In any case, an adapted POD subspace is required!!

# Example for sea wave energy converter (point absorber)



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Example for sea wave energy converter (point absorber)



**Out-of-sample ("prediction" with**  $N_r = 30$  **modes) POD basis**  $\Phi$  **built using snapshots from two "nearby" waves (in parameter space)**  Example for sea wave energy converter (point absorber)



**Out-of-sample** ("prediction" with  $N_r = 30$  modes) **POD** basis  $\Phi$  built using snapshots from two "distant" waves (in parameter space)

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Robustness of the POD subspace Sampling of the input parameter space

Distances in the solution space

**Computation of**  $\{\Phi_n\}_{n=1}^{N_r}$  $\Rightarrow$  **A robust POD subspace is required!** 

#### ▶ How to perform an efficient sampling of input parameter space?

 $\hookrightarrow$  Previous studies: Uniform Sampling in a Cartesian way. Problem: not optimal  $\hookrightarrow$  distance in parameter space  $\neq$  "distance" in solution space

#### ► Iterative sampling based on an <u>error</u> criterion (OLD)

- $\hookrightarrow$  Iterative method to improve the POD basis
- $\hookrightarrow$  The error is the mathematical projection error computed using the current POD basis
- $\hookrightarrow$  "Adaptive mesh refinement" using Delaunay triangulation (dual of Voronoi tesselation)

### ► Iterative sampling based on a <u>distance</u> criterion (NEW)

 $\hookrightarrow$  Distance between solution: steady vs. unsteady

# ► Steady problems

→ Computing the distance between steady solutions for different operating conditions is "easy" (Wasserstein distance, relative difference/error)



Distances in the solution space

 $\hookrightarrow$  We thus consider two POD basis  $\Phi_1 \in \mathbb{R}^{Nf \times N_{\Phi}}$  and  $\Phi_2 \in \mathbb{R}^{Nf \times N_{\Phi}}$ .

(The columns of  $\Phi_i$  provides a basis of a subspace  $S_i$  of dimension  $N_{\Phi}$  in  $\mathbb{R}^{N_f}$ )

Robustness of the POD subspace Sampling of the input parameter space



Principal Angles

Geodesic on the Grassmann manifold

 $\hookrightarrow$  Interpolations using angles or along the geodesic are possible

 $\hookrightarrow$  Be sure the solution to be interpolated is on (or close to) the geodesic!!

 $\hookrightarrow$  Interpolation should be performed using "quite close" points

#### **Principal Angles Between Subspaces (PABS)**

(J. Hamm & D.D. Lee, Grassmann Discriminant Analysis)

 $\hookrightarrow$  Definition: the principal angles  $0 \le \theta_1 \le \theta_2 \le \cdots \le \theta_{N_{\Phi}} \le \frac{\pi}{2}$  between two subspaces span( $\Phi_1$ ) and span( $\Phi_2$ ), are defined recursively by

 $\cos \theta_k = \max_{\boldsymbol{u}_k \in \operatorname{span}(\boldsymbol{\Phi}_1)} \max_{\boldsymbol{v}_k \in \operatorname{span}(\boldsymbol{\Phi}_2)} \boldsymbol{u}'_k \boldsymbol{v}_k,$ subject to  $u'_k u_k = v'_k v_k = 1$ , and  $u'_k u_i = v'_k v_i = 0$  (i = 1, ..., k - 1)

 $\hookrightarrow$  Practical computation via SVD:

$$\boldsymbol{\Phi}_1'\boldsymbol{\Phi}_2 = \boldsymbol{U}(\cos(\boldsymbol{\theta}))\boldsymbol{V}'$$

with  $\boldsymbol{U} = [\boldsymbol{u}_1 \ldots \boldsymbol{u}_{N_{\Phi}}], \ \boldsymbol{V} = [\boldsymbol{v}_1 \ldots \boldsymbol{v}_{N_{\Phi}}] \text{ and } \cos \boldsymbol{\theta} = \operatorname{diag}(\cos \theta_1 \ldots \cos \theta_{N_{\Phi}})$ 



Distances in the solution space

#### Principal Angles Between Subspaces (PABS)

(J. Hamm & D.D. Lee, Grassmann Discriminant Analysis)

 $\hookrightarrow$  Different Metrics are usually used

- Projection: 
$$d_P(S_1, S_2) = \left(\sum_{i=1}^{N_{\Phi}} \sin^2 \theta_i\right)^{\frac{1}{2}}$$
  
- Binet-Cauchy:  $d_{BC}(S_1, S_2) = \left(1 - \prod_i \cos^2 \theta_i\right)^{\frac{1}{2}}$ 

- Max-Min Correlation:  $d_{Max}(S_1, S_2) = \sin \theta_1$ ,  $d_{Min}(S_1, S_2) = \sin \theta_{N_{\Phi}}$ 

- Grassmann distance: 
$$d_G(S_1, S_2) = \left(\sum_{i=1}^{N_{\Phi}} \theta_i^2\right)^{\frac{1}{2}}$$

#### Geodesic on the Grassmann manifold

(D. Amsallem and C. Farhat, AIAA Journal, 2008)

- The subspace  $S_i = \operatorname{span}(\Phi_i)$  belongs to the Grassmann manifold  $\mathcal{G}(N_{\Phi}, N_f)$  $\hookrightarrow \mathcal{G}(N_{\Phi}, N_f)$  is defined as the set of all  $N_{\Phi}$ -dimensional subspaces of  $\mathbb{R}^{N_f}$
- Each  $N_{\Phi}$ -dimensional subspaces of  $\mathbb{R}^{N_f}$  can be viewed as a point on  $\mathcal{G}(N_{\Phi}, N_f)$
- It is thus possible to define distance  $d_G(S_1, S_2)$ , the geodesic between these points.
- $\hookrightarrow$  Practical computation via thin SVD:

 $(I - \Phi_1 \Phi_1') \Phi_2(\Phi_1' \Phi_2) = U \Sigma V'$  with  $\theta = \tan^{-1}(\Sigma)$ 

 $\hookrightarrow$  Can be used to perform interpolation between more than two subspaces

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Conformation				

► Goal

- $\hookrightarrow$  We want to predict the flow characteristics for  $100 \le Re \le 500$
- $\hookrightarrow$  For low numerical costs



Re = 100





# Sampling

► Sampling by continuation method on the Grassmann geodesic



Re = 125 is almost on the geodesic  $Re = 100 \leftrightarrow Re = 150!$ Almost uniform sampling in the solution space!!

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Subanagas internalati				

#### Subspaces interpolation

# ► Interpolation for one dimensional input parameter space between *s*<sub>0</sub> and *s*<sub>1</sub>

- $\hookrightarrow$  On the geodesic between two points on the Grassmann manifold  $\mathcal{S}_0$  and  $\mathcal{S}_1$
- $\hookrightarrow \mathcal{T}_{\mathcal{S}_0}$  is the tangent space to the Grassmann manifold at  $\mathcal{S}_0$
- $\hookrightarrow \chi_1$  is the geodesic initial condition given by  $\Gamma = U \tan^{-1}(\Sigma) V'$  on  $\mathcal{T}_{\mathcal{S}_0}$

where  $(I - \Phi_0 \Phi'_0) \Phi_1(\Phi'_0 \Phi_1) = U \Sigma V'$  with  $\theta = \tan^{-1}(\Sigma)$ 

 $\hookrightarrow \text{ Interpolation } \Phi(s) = \text{span} \left[ \Phi_0 V \cos \left( \frac{s-s_0}{s_1-s_0} \theta \right) + U \sin \left( \frac{s-s_0}{s_1-s_0} \theta \right) \right], s \in [s_0, s_1]$ 



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► Evolution of L<sub>2</sub> errors for snapshots projection over different POD basis



Comparison of projection errors on several basis

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	Robustness of the POD subspace	Example: cylinder wake flow vs.	Reynolds number	

# Improvement of the interpolation

- ► Potential sources of errors
- $\hookrightarrow$  Computation of direction  $\Gamma_I$  from  $\alpha$  and  $\beta$  is not adapted to the solution space
- $\hookrightarrow$  Computation of *s* along direction  $\Gamma_I$  may not be adapted too



 $\hookrightarrow$  What if one consider  $\frac{1}{\mu}$  instead of  $\mu$ ? or generally  $f(\mu)$ ? Where is the middle?

 $\Rightarrow$  Manifold learning to approximate appropriate  $s = f(\mu)$  for interpolations!

# **Conclusions & Perspectives**

# ► Sampling and interpolation

- Sampling on Grassmann manifold or PABS
  - $\hookrightarrow$  Depends on the metric used (build on Principal Angles)
- Interpolation efficient in 1D input parameter space (almost linear)
  - $\hookrightarrow$  Fine and efficient sampling  $\Rightarrow$  piecewise manifold approximation is good
- Interpolation more difficult in 2D input parameter space
  - $\hookrightarrow$  Solution for  $\frac{\mu_1 + \mu_2}{2}$  may be not on the middle geodesic (*s* = 0.5)
  - $\hookrightarrow$  Interpolation parameters ( $\alpha$  and  $\beta$ ) should respect constrains
  - $\hookrightarrow$  Idea: try to approximate the geometry of the (Grassmann) solution manifold
  - $\hookrightarrow$  Isomap (shortest paths on distance graphs) + Multi-Dimensionnal Scaling
  - Next: "dig" manifold approximation via Grassmann-MDS

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**Conclusions & Perspectives** 

- ► Multi-fidelity numerical modeling: FOM and POD ROM coupling
  - Applied to renewable energy applications (WECs and wind-turbines)
    - $\hookrightarrow "Problems" for WECs: POD of bi-fluid configurations not easy Moving front: linear approx. not adapted...$



- Snapshots clustering, then POD for each cluster (piecewise linear approx.)
- Snapshots mapping onto reference solution, then POD (non linear approx.)
  → Optimal transport (non-linear approx.), quadratic approx. (Stanford)

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