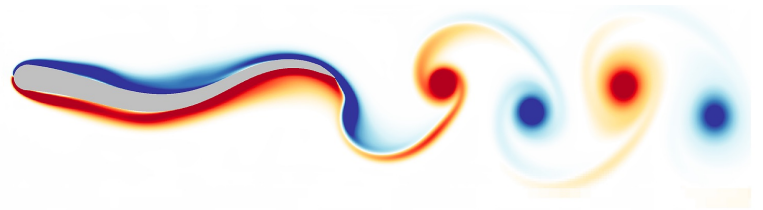




**SAN DIEGO STATE
UNIVERSITY**



Computational Fluid Dynamics and Flow Physics Laboratory

A consistent, volume preserving, and adaptive mesh refinement-based framework for modeling phase changing non-isothermal gas-liquid-solid flows

■ **Amneet Pal S. Bhalla**

Associate Professor of Mechanical Engineering

San Diego State University

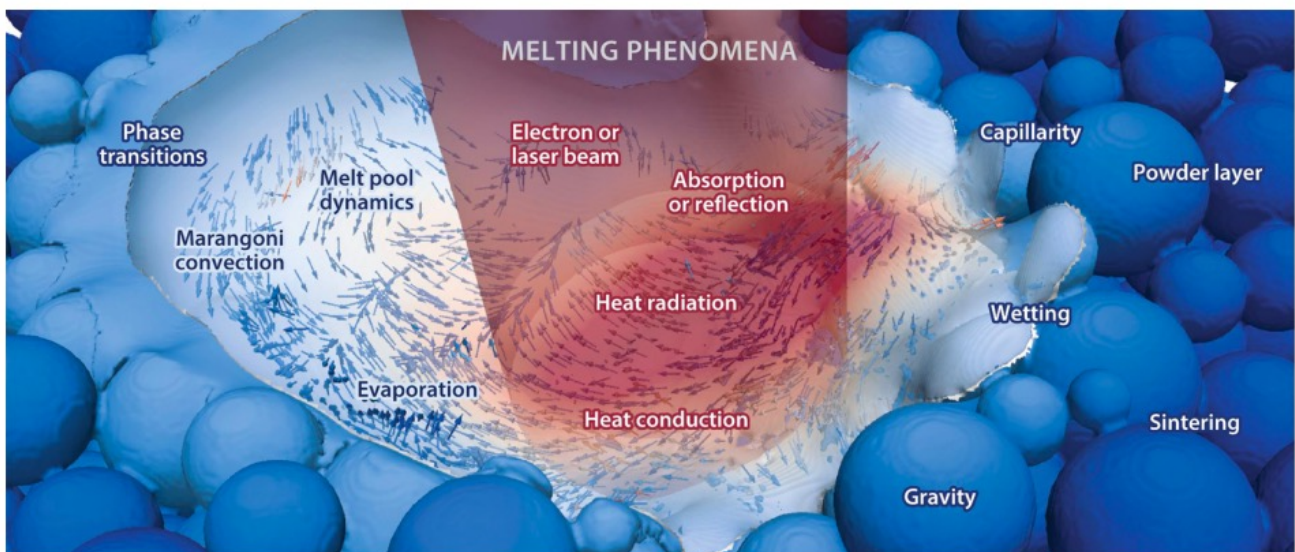
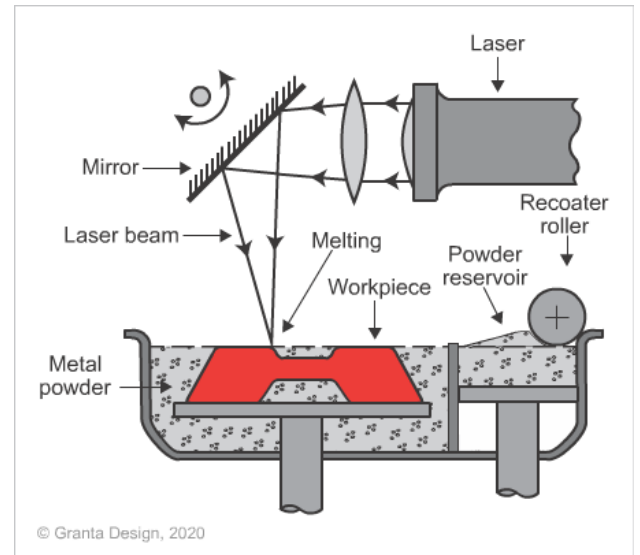
Ramakrishnan Thirumalaisamy

Ph.D. student, Department of Mechanical Engineering

San Diego State University

ICCFD 12, Kobe, Japan, 2024

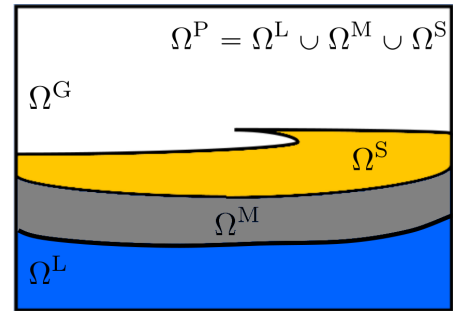
NON-ISOTHERMAL MULTIPHHASE FLOWS WITH PHASE CHANGE



A CONSISTENT MATHEMATICAL FRAMEWORK

LEVEL SET ADVECTION:

$$\frac{\phi^{n+1} - \phi^n}{\Delta t} + \mathbf{u} \cdot \nabla \phi = 0$$



HEAVISIDE ADVECTION:

$$\frac{H^{n+1} - H(\phi)^n}{\Delta t} + \nabla \cdot \phi \mathbf{u} = H \nabla \cdot \mathbf{u}$$

$$H(\phi) = \begin{cases} 1 & \text{PCM} \\ 0 & \text{Gas} \end{cases}$$

$$\varphi = \begin{cases} 1, & \text{Liquid} \\ 0, & \text{Solid} \end{cases}$$

MASS CONSERVATION:

$$\frac{\rho^{n+1} - \rho^n}{\Delta t} + \nabla \cdot m_\rho = 0$$

ENTHALPY EQUATION:

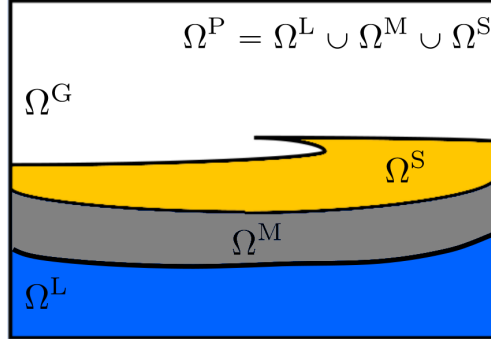
$$\frac{\rho^{n+1} h^{n+1} - (\rho h)^n}{\Delta t} + \nabla \cdot (m_\rho h) = \nabla \cdot (\kappa \nabla T) + Q_{\text{src}}$$

NAVIER STOKES SYSTEM:

$$\frac{\rho^{n+1} \mathbf{u}^{n+1} - (\rho \mathbf{u})^n}{\Delta t} + \nabla \cdot (m_\rho \mathbf{u}) = -\nabla p + \nabla \cdot [\mu (\nabla \mathbf{u} + \nabla \mathbf{u}^T)] + \rho \mathbf{g} - A_d \mathbf{u}$$

$$\nabla \cdot \mathbf{u} = -\frac{1}{\rho} \frac{D\rho}{Dt}$$

A NOVEL LOW MACH ENTHALPY METHOD



$$H = \begin{cases} 1, & \text{PCM} \\ 0, & \text{Gas} \end{cases}$$

$$\varphi = \begin{cases} 1, & \text{Liquid} \\ 0, & \text{Solid} \end{cases}$$

ENTHALPY EQUATION:

$$\frac{\rho^{n+1} h^{n+1} - (\rho h)^n}{\Delta t} + \nabla \cdot (m_\rho h) = \nabla \cdot (\kappa \nabla T) + Q_{\text{src}}$$

h – T RELATION:

$$h = \begin{cases} C^S T, & T < T^{\text{sol}}, \\ \bar{C}(T - T^{\text{sol}}) + h^{\text{sol}} + \varphi \frac{\rho^L}{\rho} L, & T^{\text{sol}} \leq T \leq T^{\text{liq}}, \\ C^L(T - T^{\text{liq}}) + h^{\text{liq}}, & T > T^{\text{liq}}, \end{cases}$$

φ – h RELATION:

$$\varphi = \begin{cases} 0, & h < h^{\text{sol}}, \\ \frac{\rho^S (h^{\text{sol}} - h)}{h(\rho^L - \rho^S) - \rho^L h^{\text{liq}} + \rho^S h^{\text{sol}}}, & h^{\text{sol}} \leq h \leq h^{\text{liq}}, \\ 1, & h > h^{\text{liq}}. \end{cases}$$

EQUATION OF STATE:

$$\rho = \rho^G + (\rho^S - \rho^G)H + (\rho^L - \rho^S)H\varphi$$

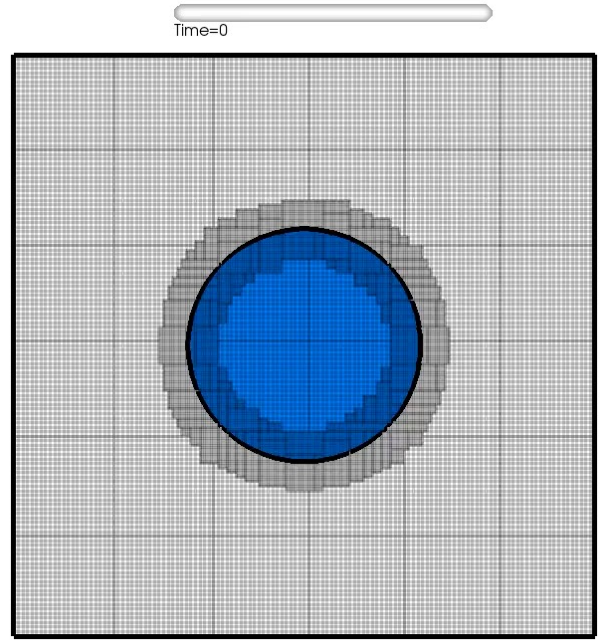
LOW MACH EQUATION:

$$\nabla \cdot \mathbf{u} = -\frac{1}{\rho} \frac{D\rho}{Dt}$$

$$\nabla \cdot \mathbf{u} = -\frac{\rho^S \rho^L}{\rho^2} (\rho^L - \rho^S) H \frac{(h^{\text{liq}} - h^{\text{sol}})}{(h(\rho^L - \rho^S) - \rho^L h^{\text{liq}} + \rho^S h^{\text{sol}})^2} (\nabla \cdot \kappa \nabla T)$$

CONSISTENT TIME INTEGRATORS

- The use of the same mass flux \mathbf{m}_p in various transport equations ensures numerical stability for high density ratio flows
- **Option 1:** Use the same time integration scheme for mass, momentum and enthalpy equations.
- **Option 2:** Include additional stabilizing terms (shown in red below) in the momentum and energy equations.



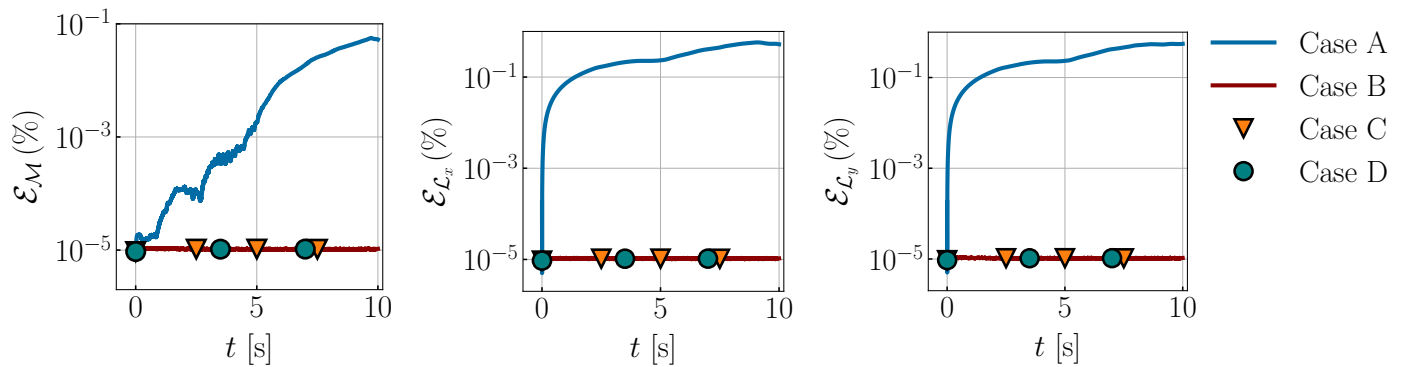
Test problem: isothermal advection of a dense bubble in inviscid gas

$$\rho_i/\rho_o = 10000 \quad (u, v) = (1, 1)$$

$$\frac{\check{\rho}^{n+1,k+1} \mathbf{u}^{n+1,k+1} - \check{\rho}^n \mathbf{u}^n}{\Delta t} + \mathbf{C} \left(\mathbf{u}_{\text{adv}}^{(2)}, \check{\rho}_{\text{lim}}^{(2)} \mathbf{u}_{\text{lim}}^{(2)} \right) = \mathcal{R} \mathbf{u}^{n+1,k} + \text{viscous} + \text{pressure} + \text{other forces}$$

$$\frac{\check{\rho}^{n+1,k+1} h^{n+1,k+1} - \check{\rho}^n h^n}{\Delta t} + A \left(h_{\text{lim}}^{(1)}, \check{\rho}_{\text{lim}}^{(1)} \mathbf{u}_{\text{adv}}^{(1)} \right) = \mathcal{R} h^{n+1,k} + (\nabla \cdot \kappa \nabla T)^{n+1,k+1} + Q_{\text{src}}^{n+1,k}$$

IMPORTANCE OF CONSISTENT INTEGRATORS



RK-2 integrator is employed for the momentum equation in all 4 cases

Case A: SSP-RK3 integrator for mass equation.

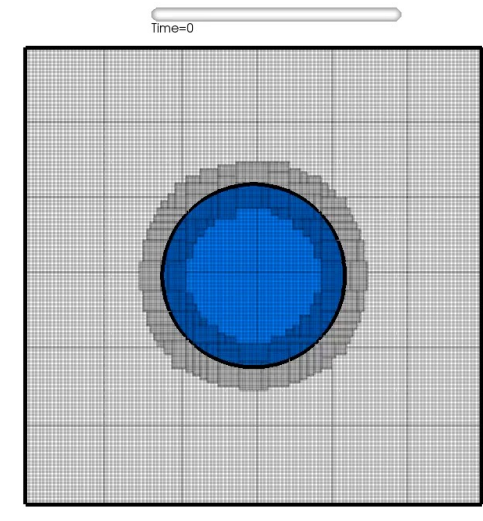
Case B: SSP-RK3 integrator for mass equation, and residual force in the momentum equation.

Case C: RK-2 integrator for mass equation.

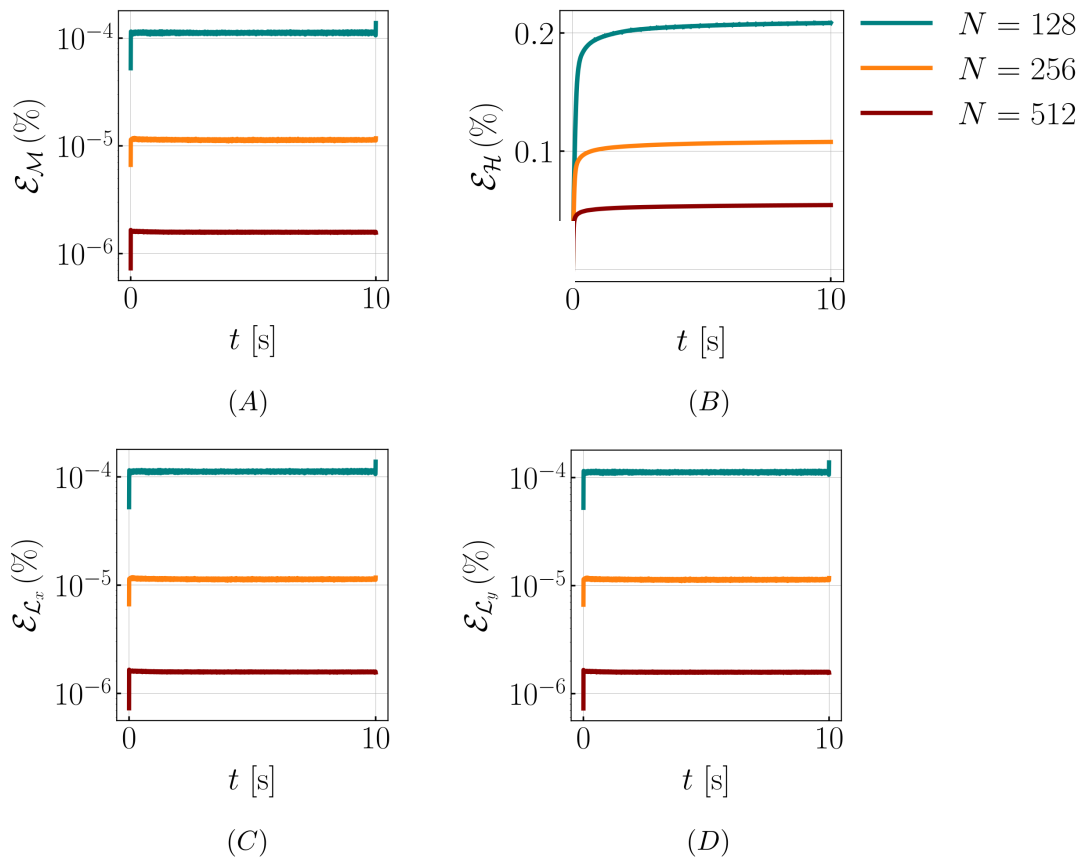
Case D: RK-2 integrator for mass equation, and residual force in the momentum equation

Cases B, C and D preserve momentum, enthalpy and phase of the system.

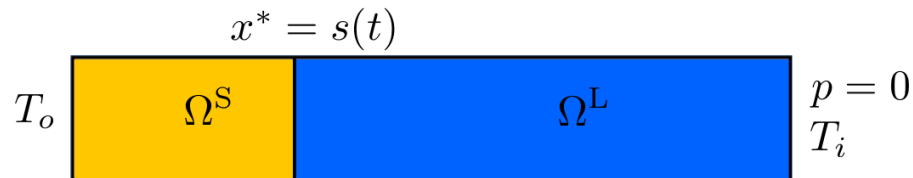
GRID CONVERGENCE STUDY



Test problem: isothermal advection of a dense bubble in inviscid gas



SOLVING TWO PHASE STEFAN PROBLEM WITH DENSITY JUMP



SOLIDIFICATION PROBLEM

Heat equations

$$\rho^S C^S \frac{\partial T^S}{\partial t} = \kappa^S \frac{\partial^2 T^S}{\partial x^2} \in \Omega^S(t),$$

$$\rho^L C^L \left(\frac{\partial T^L}{\partial t} + u^L \frac{\partial T^L}{\partial x} \right) = \kappa^L \frac{\partial^2 T^L}{\partial x^2} \in \Omega^L(t)$$

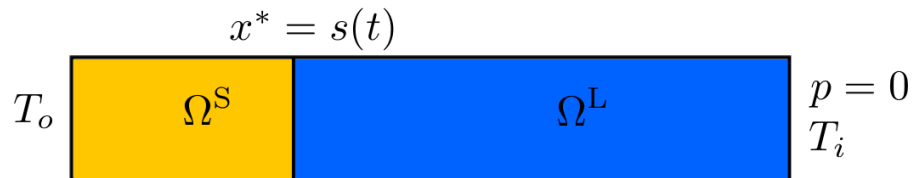
Stefan condition

$$\rho^S \left[(C^L - C^S)(T_m - T_r) + L - \frac{1}{2}(1 - R_\rho^2) \left(\frac{ds}{dt} \right)^2 \right] \frac{ds}{dt} = \left(\kappa^S \frac{\partial T^S}{\partial x} - \kappa^L \frac{\partial T^L}{\partial x} \right)_{x^*}.$$

$$R_\rho = \rho^S / \rho^L$$

Josef Stefan	
	
Born	24 March 1835 St. Peter (today in Klagenfurt), Austrian Empire
Died	7 January 1893 (aged 57) Vienna, Austria-Hungary
Alma mater	University of Vienna
Known for	Stefan–Boltzmann law Stefan–Boltzmann constant Stefan problem Stefan's equation Stefan's formula Stefan flow Stefan number Maxwell–Stefan diffusion Squeeze flow
Awards	Lieben Prize (1865)
Scientific career	
Fields	Physicist
Institutions	University of Vienna
Academic advisors	Andreas von Ettingshausen
Doctoral students	Ludwig Boltzmann Marian Smoluchowski Johann Josef Loschmidt

SOLVING TWO PHASE STEFAN PROBLEM WITH DENSITY JUMP



SOLIDIFICATION PROBLEM

$$\rho^S C^S \frac{\partial T^S}{\partial t} = \kappa^S \frac{\partial^2 T^S}{\partial x^2} \in \Omega^S(t),$$

Heat equations

$$\rho^L C^L \left(\frac{\partial T^L}{\partial t} + u^L \frac{\partial T^L}{\partial x} \right) = \kappa^L \frac{\partial^2 T^L}{\partial x^2} \in \Omega^L(t)$$

$$\rho^S \left[(C^L - C^S)(T_m - T_r) + L - \frac{1}{2}(1 - R_\rho^2) \left(\frac{ds}{dt} \right)^2 \right] \frac{ds}{dt} = \left(\kappa^S \frac{\partial T^S}{\partial x} - \kappa^L \frac{\partial T^L}{\partial x} \right)_{x^*}.$$

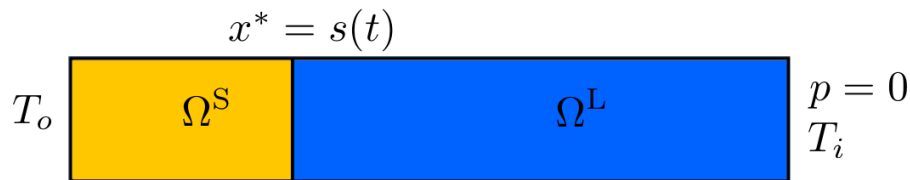
Stefan condition

$$R_\rho = \rho^S / \rho^L$$

Terms in red boxes pertain to density jumps.
These are ignored in the literature.
We consider them.

Josef Stefan	
	
Born	24 March 1835 St. Peter (today in Klagenfurt), Austrian Empire
Died	7 January 1893 (aged 57) Vienna, Austria-Hungary
Alma mater	University of Vienna
Known for	Stefan–Boltzmann law Stefan–Boltzmann constant Stefan problem Stefan's equation Stefan's formula Stefan flow Stefan number Maxwell–Stefan diffusion Squeeze flow
Awards	Lieben Prize (1865)
Fields	Scientific career Physicist
Institutions	University of Vienna
Academic advisors	Andreas von Ettingshausen
Doctoral students	Ludwig Boltzmann Marian Smoluchowski Johann Josef Loschmidt

SOLVING TWO PHASE STEFAN PROBLEM



SOLIDIFICATION PROBLEM

Analytical solution:

$$T^S = T_o + (T_m - T_o) \operatorname{erf} \left(\frac{x}{2\sqrt{\alpha^S t}} \right) / \operatorname{erf} \left(\lambda(t) \sqrt{\frac{\alpha^L}{\alpha^S}} \right)$$

$$T^L = T_i + (T_m - T_i) \frac{\operatorname{erfc} \left(\frac{x}{2\sqrt{\alpha^L t}} - \lambda(t) (1 - R_\rho) \right)}{\operatorname{erfc} (\lambda(t) R_\rho)}$$

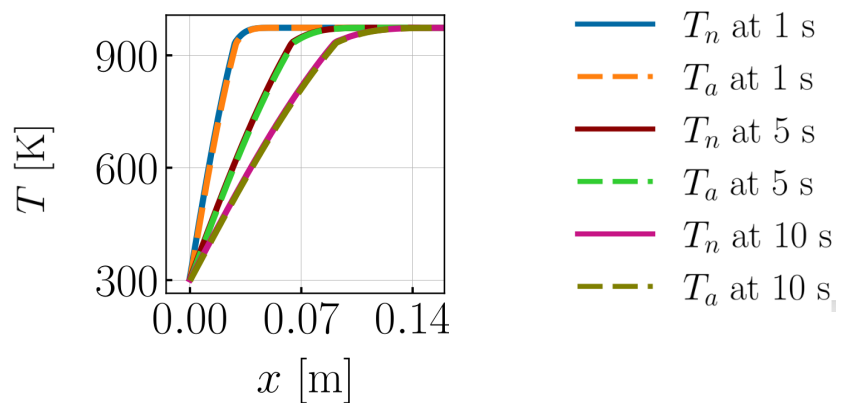
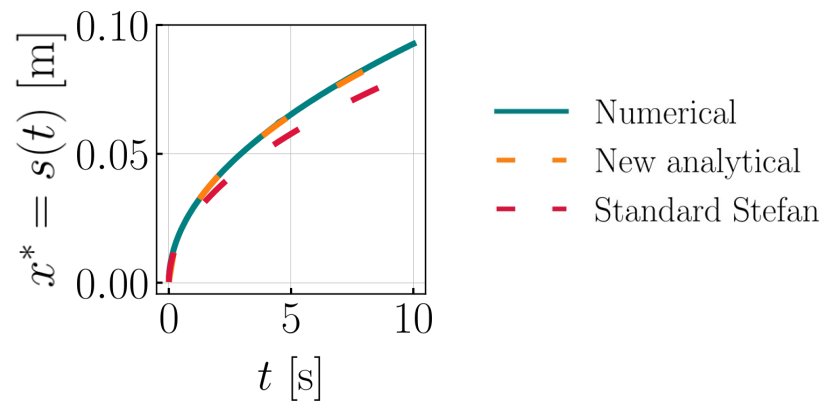
Transcendental equation for λ :

$$\rho^S \left[L^{\text{eff}} - \frac{(1 - R_\rho^2)}{2} \left(\frac{\lambda^2 \alpha^L}{t} \right) \right] \lambda \sqrt{\alpha^L} = \kappa^S \frac{T_m - T_o}{\operatorname{erf} \left(\lambda \sqrt{\frac{\alpha^L}{\alpha^S}} \right)} \frac{e^{-\lambda^2 \alpha^L / \alpha^S}}{\sqrt{\pi \alpha^S}} + \kappa^L \frac{T_m - T_i}{\operatorname{erfc} (\lambda R_\rho)} \frac{e^{-\lambda^2 R_\rho^2}}{\sqrt{\pi \alpha^L}}$$



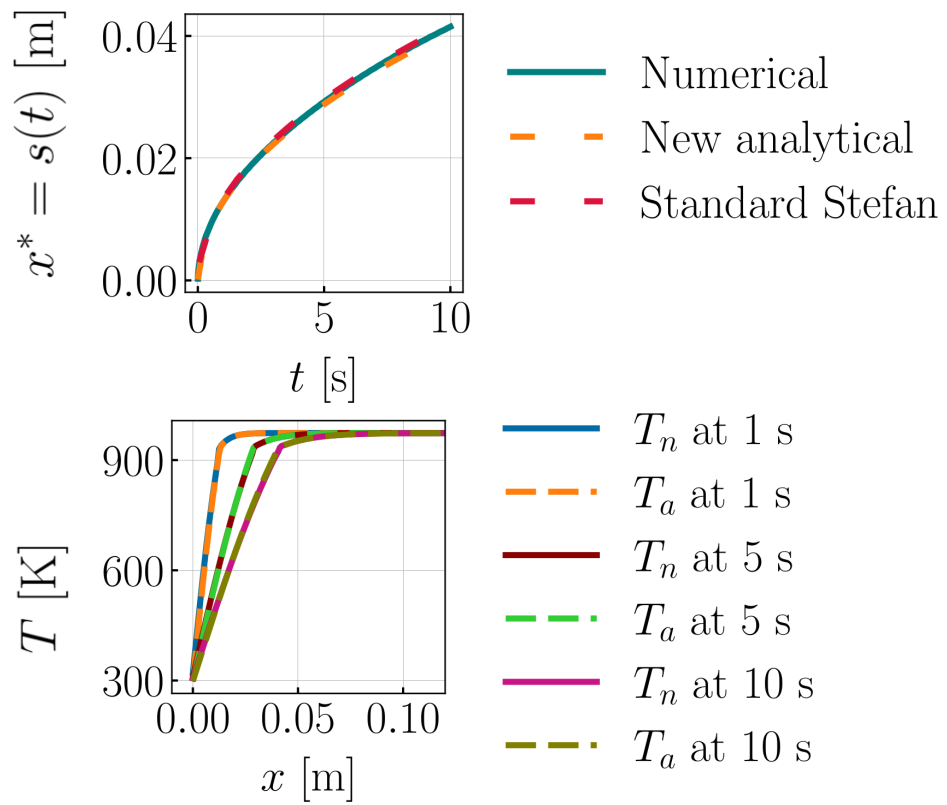
STEFAN PROBLEM WITH DENSITY DIFFERENCE

Expansion $\rho^S/\rho^L < 1$



STEFAN PROBLEM WITH DENSITY DIFFERENCE

Shrinkage $\rho^S/\rho^L > 1$

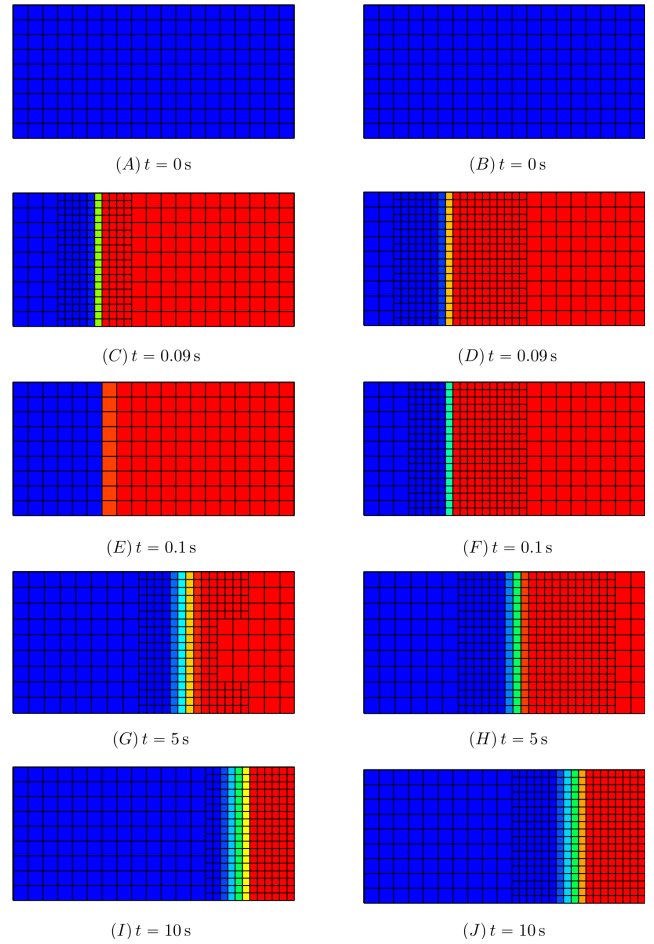
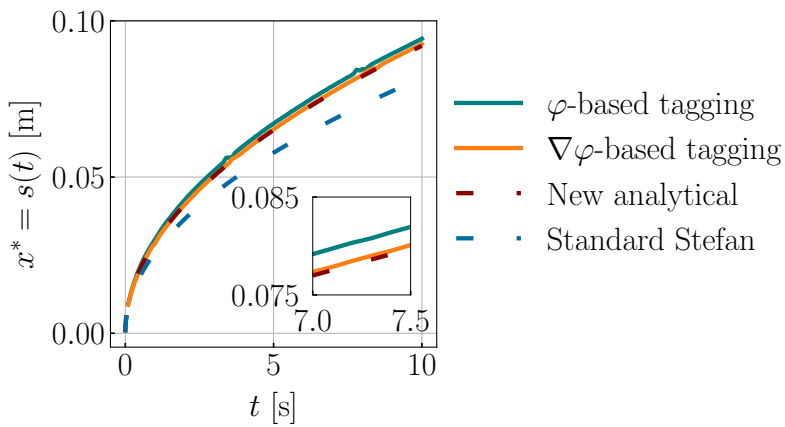


ADAPTIVE MESH REFINEMENT

PCM-gas interface: Tagging cells based on the signed distance function

Liquid-solid interface:

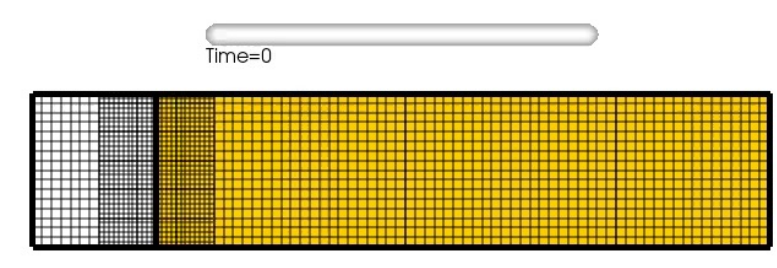
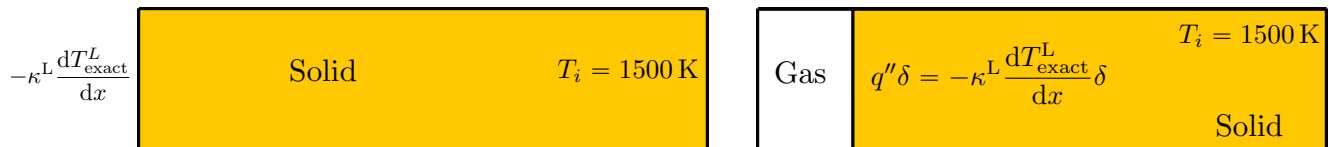
1. φ -based tagging
2. $\nabla\varphi$ -based tagging



LASER-INDUCED MELTING OF METALS WITH VOLUME CHANGE

Numerical studies have relied on experimental data to validate heat source (e.g., laser beams) induced melting of metals and alloys.

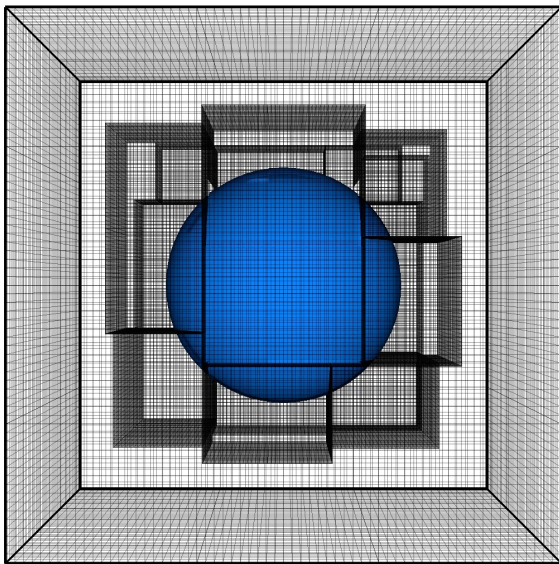
We use two phase Stefan analytical solution to validate heat source-induced melting of metals in presence of gas.



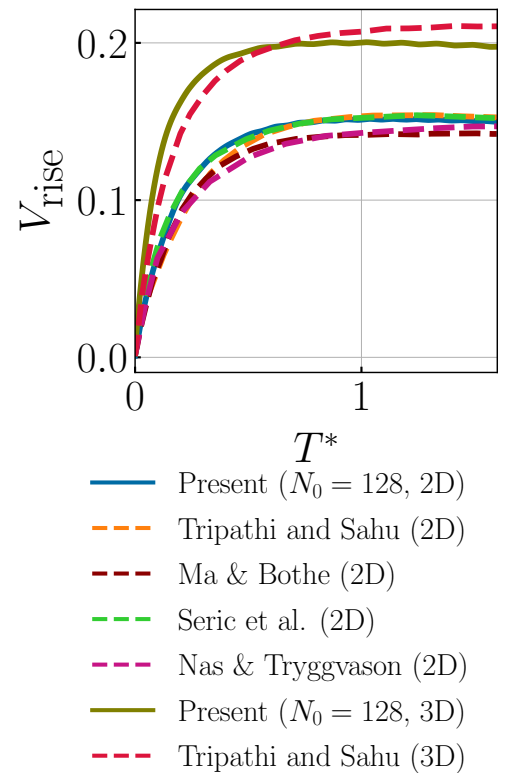
THERMOCAPILLARY FLOWS WITH LOW MACH ENTHALPY METHOD

$$\mathbf{f}_{\text{st}} = \sigma \kappa \mathbf{n} \delta + \nabla_{\parallel} \sigma \delta$$

$$\sigma = \sigma_0 + \left. \frac{d\sigma}{dT} \right|_0 (T - T_0)$$



We solve the enthalpy equation
(not temperature)



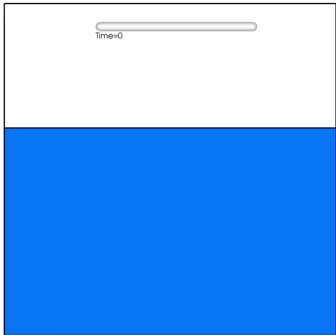
$$Re = Ma = 0.72, Ca = 0.0576$$

SIMULATING METAL CASTING DEFECTS

Pipe shrinkage

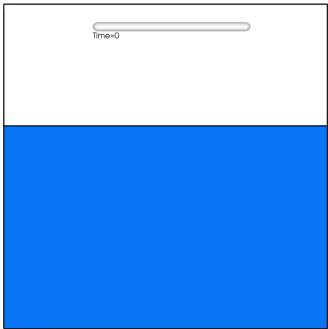


$$\rho^S > \rho^L$$






Shrinkage defect

$$\rho^S < \rho^L$$

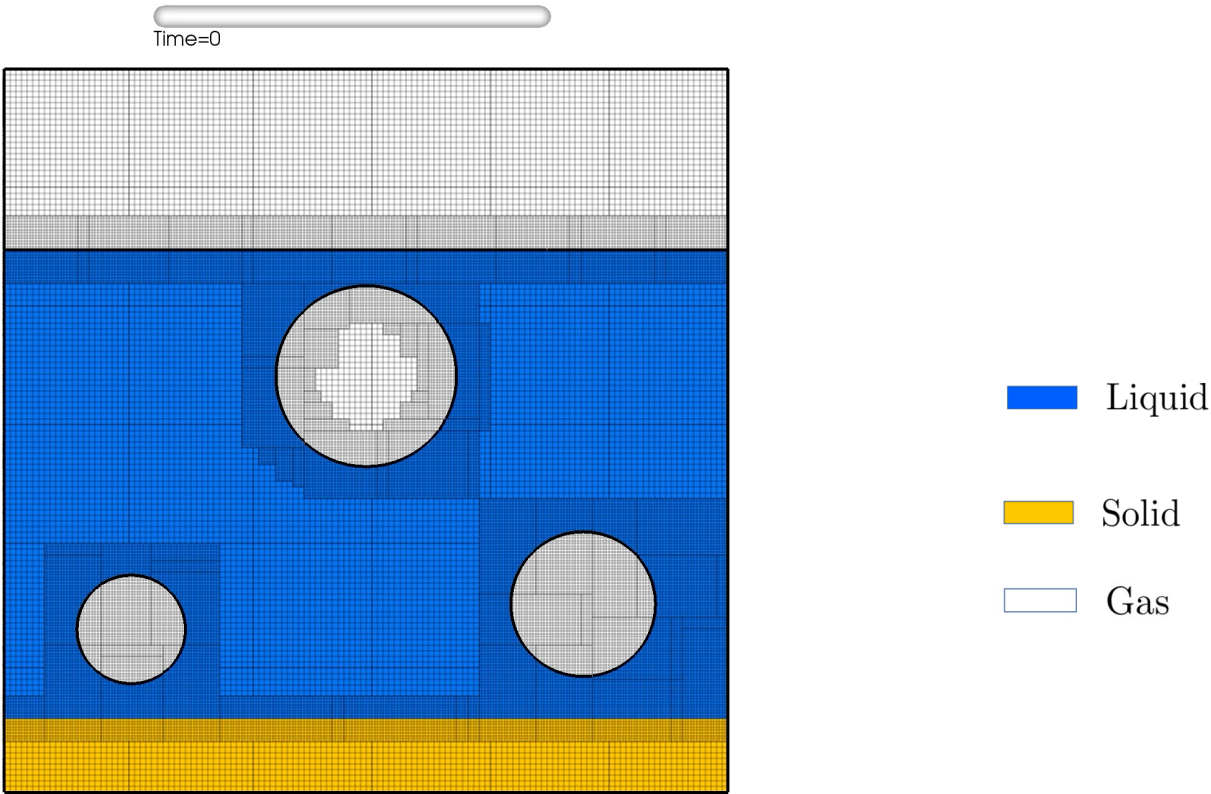


Protrusion defect

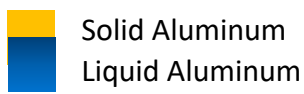
-  Liquid
-  Solid
-  Gas

Ludwig, A., Wu, M. and Kharicha, A., 2016. Simulation in metallurgical processing: Recent developments and future perspectives. *JOM*, 68, pp.2191-2197.

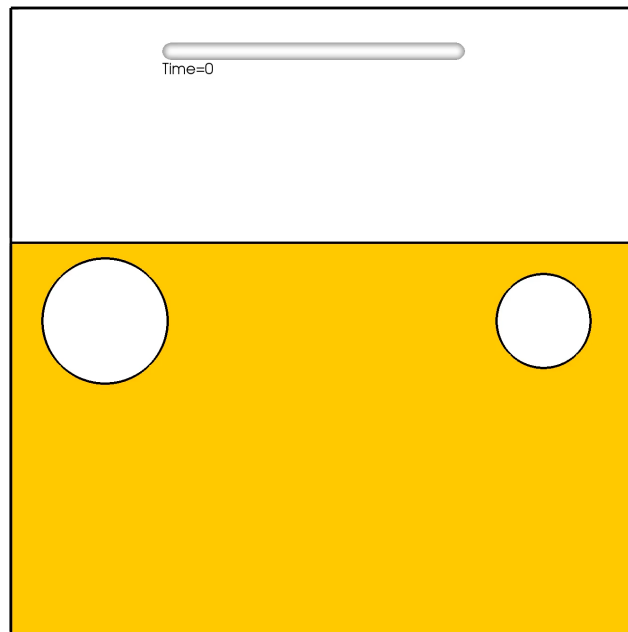
SIMULATING POROSITY DEFECTS



MELTING AND RE-SOLIDIFICATION OF ALUMINUM (SURFACE TENSION EFFECTS)

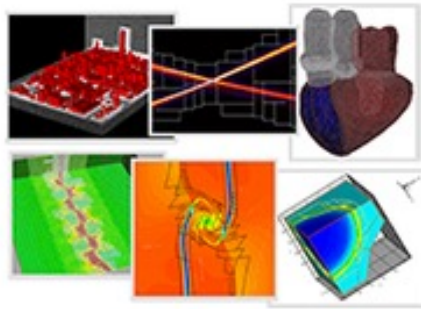


$$\begin{aligned} T > T_M & \quad t \leq 0.2 \\ T = T_M & \quad t > 0.2 \end{aligned}$$



$$\begin{aligned} T > T_M & \quad t \leq 0.2 \\ T = T_M & \quad t > 0.2 \end{aligned}$$

IMPLEMENTATION



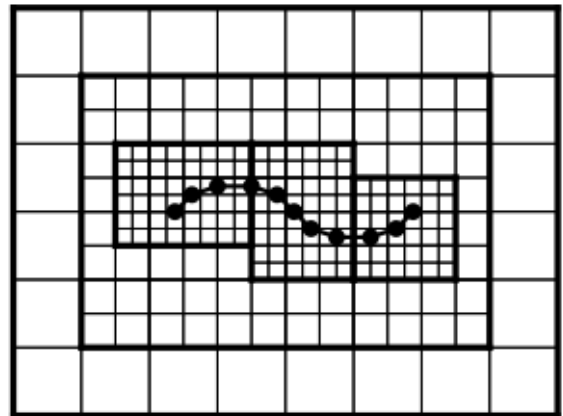
SAMRAI

$$Ax = b$$

PETSc

IBAMR

<https://github.com/IBAMR/IBAMR>



IBAMR is a distributed-memory (MPI) parallel implementation of the immersed boundary (IB) method with support for Cartesian grid adaptive mesh refinement (AMR). Written in C++ and Fortran.

REFERENCES

1. R. Thirumalaisamy, K. Khedkar, P. Ghysels, **A. P. S. Bhalla**, 2023, An effective preconditioning strategy for volume penalized incompressible multiphase flow solvers, *Journal of Computational Physics*, Vol. 490, 112325.
2. R. Thirumalaisamy, **A. P. S. Bhalla**, 2023, A low Mach enthalpy method to model non-isothermal gas-liquid-solid flows with melting and solidification, *International Journal of Multiphase Flow*, vol. 169, 104605.
3. N. Nangia, B. E. Griffith, N. A. Patankar, and **A. P. S. Bhalla**. "A robust incompressible Navier-Stokes solver for high density ratio multiphase flows." *Journal of Computational Physics* 390 (2019): 548-594.
4. R. Thirumalaisamy, **A. P. S. Bhalla**, 2024, A consistent, volume preserving, and adaptive mesh refinement-based framework for modeling non-isothermal gas-liquid-solid flows with phase change (submitted).

FUNDING AND ACKNOWLEDGEMENTS

NSF OAC 1931368, NSF CBET CAREER 2234387, DOE ECP 17-SC-20-SC



QUESTIONS / COMMENTS?

